Frequency Tracking with the Histogram-PMHT Algorithm

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FREQUENCY TRACKING WITH HISTOGRAM-PMHT

1. INTRODUCTION

Tracking an unknown, nonstationary signal in time and frequency against a noisy, non-stationary background on an intensity-modulated sensor display is a difficult problem. Traditional techniques involve thresholding the sensor data and treating the exceedences as point measurements that are subsequently fed to a tracking algorithm. Choosing this threshold is a challenge in itself, and even then it is typically subject to a prescribed probability of detection and probability of false alarm. In reference 1, Streit derives a new tracking algorithm that uses all of the senor data, and thus avoids thresholding entirely. The fundamental premise of this tracking algorithm is that losses due to thresholding the sensor data can be eliminated completely if all of the sensor data are used by the tracking algorithm.

Section 2 describes this new tracking algorithm, referred to herein as histogram probabilistic multi-hypothesis tracking, or histogram-PMHT; in particular, the key aspects of its derivation are discussed. A concise statement of the histogram-PMHT algorithm applied to frequency tracking is given in section 3. Two examples, one involving a simulated linear chirp, and one involving a bowhead whale call recorded at sea, are presented in section 4. A summary is given in section 5.

2. HISTOGRAM-PMHT

2.1 SIGNAL AND MEASUREMENT MODELS

The histogram-PMHT tracking algorithm is intrinsically a multi-signal tracking algorithm, and is based on a stochastic model of the signals and the noise background. It assumes that the signals and the noise background are described by a discrete mixture of continuous distributions in which the noise background and each signal are represented by a unique component, or set of components, in the mixture. The sensor data are indirect manifestations or realizations of this underlying distribution. Since in most practical applications the sensor display has a fixed resolution with a finite number of cells (e.g., discrete Fourier transform (DFT) bins in a time-frequency "waterfall" display), a discrete distribution is required to model the sensor data. The approach taken in histogram-PMHT is first to quantize the real-valued sensor data into a "pseudo-histogram," and then to use a multinomial distribution to model the counts in the histogram cells. The cell-level intensities of the sensor data are directly proportional to the cell counts of this pseudo-histogram. The goal is to fit the underlying mixture distribution to this pseudo-histogram at each scan; that

is, to estimate the parameters of the mixture distribution that maximize the likelihood of the pseudo-histogram at each scan. The theoretical framework of PMHT (see reference 2) is used to "assign" the pseudo-histogram samples to the mixture components, and to link these mixture distributions across scans with a dynamical signal model.

2.2 EXPECTATION-MAXIMIZATION

The expectation-maximization (EM) method formalized by Dempster, Laird, and Rubin (see reference 3) is a powerful method for estimating the parameters of mixture distributions, and is the method used to solve the likelihood equation in histogram-PMHT. The method of EM is particularly well suited to so-called "missing" data problems; that is, problems in which the parameters of interest are comparatively straightforward to estimate if the observed data set is augmented with certain unobserved data. The basic strategy of EM is to include the missing data as random variables in the likelihood function, take the expectation of the log-likelihood with respect to the missing data conditioned on the observed data, and maximize the resulting expression, termed the auxiliary function. The EM method requires both the specification of the incomplete (observed) data likelihood function, and the complete data (observed data plus missing data) likelihood function. The incomplete- and complete-data likelihood functions for histogram-PMHT are described in the next two sections.

2.3 INCOMPLETE-DATA LIKELIHOOD FUNCTION

Let Z_t denote the sensor-data measurement vector at time t,

$$Z_t = \{z_{t1}, \dots, z_{tL}\}, \qquad t = 1, \dots, T,$$
 (2.1)

where $z_{t\ell}$ is the output of the sensor at time t in display cell ℓ (unaveraged, short-time, magnitude-squared Fourier transform data versus frequency bins in this application). Let $\hbar^2 > 0$ be a specified quantization level, and let

$$N_t = \{n_{t1}, \dots, n_{tL}\}, \qquad t = 1, \dots, T,$$
 (2.2)

denote the quantized measurement vector corresponding to Z_t , where

$$n_{t\ell} = \left\lfloor \frac{z_{t\ell}}{\hbar^2} \right\rfloor \tag{2.3}$$

is the greatest integer less than or equal to z_{tt}/\hbar^2 . Let

$$N_{t\Sigma} = \sum_{\ell=1}^{L} n_{t\ell} \tag{2.4}$$

denote the total cell count (sample size) at time t. The quantized data vector N_t is used as an intermediate variable in the derivation of the histogram-PMHT algorithm; at an appropriate point in the derivation, the measurement vector Z_t is recovered in the limit as $\hbar^2 \to 0$.

It is assumed that the quantized data vector N_t has a multinomial distribution consisting of $N_{t\Sigma}$ independent draws (with replacement) on L "categories" with probabilities

$$\frac{P_{\ell}(X_t)}{P(X_t)}, \qquad \ell = 1, \dots, L, \tag{2.5}$$

where

$$P_{\ell}(X_t) = \int_{\ell} f(\tau; X_t) d\tau, \qquad (2.6)$$

and

$$P(X_t) = \sum_{\ell=1}^{L} P_{\ell}(X_t). \tag{2.7}$$

In equation (2.6), $f(\tau; X_t)$ is the underlying mixture density of the signals and the background noise, and X_t denotes the parameter vector of the mixture density at time t (minus the mixing proportions, which are implicit in all of the likelihood expressions in the sequel). The assumption of a multinomial distribution for the quantized data vector N_t implies that the counts N_t form a histogram with L cells and a sample size of $N_{t\Sigma}$, where the samples are independent and identically distributed with probability density function $f(\tau; X_t)$ (see reference 4 for more on the multinomial distribution).

Let $N = \{N_1, \ldots, N_T\}$ denote the collection of quantized measurement vectors, and let $X = \{X_1, \ldots, X_T\}$ denote the set of mixture parameters to be estimated. Assuming the scans are independent, the incomplete data likelihood function for N is given by

$$p_{inc}(N;X) = \prod_{t=1}^{T} p_{inc}(N_t;X_t),$$
 (2.8)

where

$$p_{inc}(N_t; X_t) = \frac{N_{t\Sigma}!}{n_{t1}! \cdots n_{tL}!} \prod_{\ell=1}^{L} \left[\frac{P_{\ell}(X_t)}{P(X_t)} \right]^{n_{t\ell}}.$$
 (2.9)

In reference 1, a Bayesian model for the mixture parameters X is adopted. If $p_{\Xi}(X)$ denotes the a priori density of X, then the incomplete data likelihood function is given by

$$p_{inc}(N,X) = p_{\Xi}(X) p_{inc}(N|X), \qquad (2.10)$$

where the density $p_{inc}(N|X)$ is essentially identical to the density (2.8), and differs only in its statistical interpretation (Bayesian conditioning versus parametric dependence). The derivation of the prior density $p_{\Xi}(X)$ is an important theoretical development in histogram-PMHT. In short, the prior needs to be sufficiently non-diffuse so that the synthetically generated histogram counts N, which depend on the arbitrary quantization level \hbar^2 , do not overwhelm the prior as $\hbar^2 \to 0$. Under the usual Markov assumption on the signal states X_t , Bayes Theorem gives

$$p_{\Xi}(X) = p_{\Xi_0}(X_0) \prod_{t=1}^{T} [p_{\Xi_t \mid \Xi_{t-1}}(X_t \mid X_{t-1})]^{N_{t\Sigma}}, \qquad (2.11)$$

where the power of $N_{t\Sigma}$ is necessary to account for the artificial abundance of quantized data N_t at each scan.

2.4 COMPLETE-DATA LIKELIHOOD FUNCTION

The missing data in histogram-PMHT are (1) the locations of the samples that make up the pseudo-histogram, and (2) their mixture component assignments, that is, the components in the underlying mixture distribution from which the samples are drawn.

Let $\zeta_{t\ell} = \{\zeta_{t\ell 1}, \ldots, \zeta_{t\ell n_{t\ell}}\}$ denote the locations of the samples within cell ℓ . The random variables in $\zeta_{t\ell}$ are assumed to be independent and identically distributed with probability density function $f(\tau|X_t)/P_{\ell}(X_t)$. Furthermore, let $\zeta_t = \{\zeta_{t1}, \ldots, \zeta_{tL}\}$ and $\zeta = \{\zeta_1, \ldots, \zeta_T\}$.

The sample density is assumed to be the mixture density

$$f(\tau|X_t) = \sum_{k=0}^{M} \pi_{tk} G_k(\tau|X_t), \qquad (2.12)$$

where the mixing proportions $\pi_{tk} \geq 0$ for all t and k, $\sum_{k=0}^{M} \pi_{tk} = 1$ for all t, and the $G_k(\tau|X_t)$ are themselves probability density functions. For component $\pi_{t0} G_0(\tau|X_t)$, π_{t0} represents the fraction of the total power due to the background noise, and $G_0(\tau|X_t)$ models the cell-to-cell variation of the background noise. Likewise, for components $\pi_{t1} G_1(\tau|X_t), \ldots, \pi_{tM} G_M(\tau|X_t)$, π_{tk} is the fraction of the total power due to signal k, and $G_k(\tau|X_t)$ models the variation of signal k from cell to cell. The mixture model (2.12) assumes that the signal power levels may be spread across more than one cell of the sensor display.

Let $K_{t\ell} = \{k_{t\ell 1}, \ldots, k_{t\ell n_{t\ell}}\}$ denote the components of the mixture that generated the missing variables $\zeta_{t\ell} = \{\zeta_{t\ell 1}, \ldots, \zeta_{t\ell n_{t\ell}}\}$. It is assumed that the random variables in $K_{t\ell}$ are independent and identically distributed. Furthermore, let $K_t = \{K_{t1}, \ldots, K_{tL}\}$ and $K = \{K_1, \ldots, K_T\}$.

Including the missing sample locations and their mixture component assignments, the complete data likelihood function is given by

$$p_{com}(N,\zeta,K,X) = p_{\Xi}(X) \prod_{t=1}^{T} \prod_{\ell=1}^{L} \prod_{r=1}^{n_{t\ell}} f_{k_{t\ell r}}(\zeta_{t\ell r}|X_t), \qquad (2.13)$$

where

$$f_k(\tau|X_t) = \pi_{tk} G_k(\tau|X_t); \tag{2.14}$$

that is, the complete data likelihood function is the product of all the histogram sample densities across all L cells and all T scans, scaled by the prior for the signal mixture parameters.

2.5 E-STEP

The auxiliary function of the EM method, denoted here by Ψ , is defined as the conditional expectation with respect to the missing data of the logarithm of the complete data likelihood function given the observed data and the current values of the parameters X, denoted X':

$$\Psi(X, X') = E_{\zeta K}[\log p_{com}(N, \zeta, K, X) \mid N, X'], \qquad (2.15)$$

where $E_{\zeta K}$ denotes expectation with respect to the missing data. The mechanics of the E-step for histogram-PMHT are tedious but straightforward, and are well documented in reference 1. The final result in terms of the pseudo-histogram counts N is

$$\Psi(X, X') = \log p_{\Xi_0}(X_0) + \sum_{t=1}^{T} \frac{N_{t\Sigma}}{P(X'_t)} \log p_{\Xi_t|\Xi_{t-1}}(X_t|X_{t-1})$$

$$+ \sum_{t=1}^{T} \sum_{\ell=1}^{L} \sum_{k=0}^{M} \frac{n_{t\ell}}{P_{\ell}(X'_t)} \int_{\ell} f_k(\tau|X'_t) \log f_k(\tau|X_t) d\tau. \quad (2.16)$$

It is easily shown that by taking the limit

$$\Psi^{\sharp} = \lim_{\hbar^2 \to 0} \hbar^2 \Psi, \tag{2.17}$$

and using definition (2.3) for the quantization, the EM auxiliary function Ψ can be replaced by Ψ^{\sharp} , a function of the unquantized sensor data $Z = \{Z_1, \ldots, Z_t\}$:

$$\Psi^{\sharp}(X, X') = \sum_{t=1}^{T} \frac{\|Z_{t}\|}{P(X'_{t})} \log p_{\Xi_{t}|\Xi_{t-1}}(X_{t}|X_{t-1}) + \sum_{t=1}^{T} \sum_{\ell=1}^{L} \sum_{k=0}^{M} \frac{z_{t\ell}}{P_{\ell}(X'_{t})} \int_{\ell} f_{k}(\tau|X'_{t}) \log f_{k}(\tau|X_{t}) d\tau, \quad (2.18)$$

where $||Z_t|| = \sum_{\ell=1}^L z_{t\ell}$ is the L_1 -norm of Z_t .

2.6 M-STEP

The objective of the M-step is to maximize the auxiliary function Ψ^{\sharp} with respect to the unknown signal parameters X. To proceed, application-specific terms in the auxiliary function (2.18) must be defined.

Let

$$X_t = \{x_{t0}, x_{t1}, \dots, x_{tM}\}, \qquad t = 0, 1, \dots, T, \tag{2.19}$$

where x_{t0} is the background noise parameter at time t, and x_{tk} is the parameter of signal k at time t. Assuming the signals are independent at all times,

$$p_{\Xi_{t}|\Xi_{t-1}}(X_{t}|X_{t-1}) = \prod_{k=0}^{M} p_{\Xi_{tk}|\Xi_{t-1,k}}(x_{tk}|x_{t-1,k}).$$
(2.20)

It is readily shown that Ψ^{\sharp} can be separated into two terms, one involving the unknown mixing proportions $\pi = \{\pi_{tk}\}$, and one involving the unknown signal parameters X,

$$\Psi^{\sharp} = \sum_{t=1}^{T} \Psi_{t\pi} + \sum_{k=0}^{M} \Psi_{kX}, \tag{2.21}$$

where

$$\Psi_{t\pi} = \sum_{k=0}^{M} \left[\sum_{\ell=1}^{L} \frac{z_{t\ell}}{P_{\ell}(X_{t}')} \int_{\ell} G_{k}(\tau | x_{tk}') d\tau \right] \pi_{tk}' \log \pi_{tk}, \tag{2.22}$$

and

$$\Psi_{kX} = \sum_{t=1}^{T} \frac{\|Z_{t}\|}{P(X'_{t})} \log p_{\Xi_{tk}|\Xi_{t-1,k}}(x_{tk}|x_{t-1,k}) + \sum_{t=1}^{T} \sum_{\ell=1}^{L} \frac{\pi'_{tk} z_{t\ell}}{P_{\ell}(X'_{t})} \int_{\ell} G_{k}(\tau|x'_{tk}) \log G(\tau|x_{tk}) d\tau. \quad (2.23)$$

The updated mixing proportions π_t are easily obtained at each time t by maximizing with respect to π_t the Lagrangian equation involving $\Psi_{t\pi}$ and the constraint $\pi_{t0} + \pi_{t1} + \cdots + \pi_{tM} = 1$.

For this application, linear Gauss-Markov processes are assumed for the signals, so that for k = 1, ..., M and t = 1, ..., T, the signal process models are given by

$$p_{\Xi_{tk}|\Xi_{t-1,k}}(x_{tk}|x_{t-1,k}) = \mathcal{N}(x_{tk}; F_{t-1,k}|x_{t-1,k}, Q_{t-1,k}), \qquad (2.24)$$

where $\mathcal{N}(\tau; \mu, C)$ denotes the multivariate normal probability density function with mean μ and covariance matrix C, the $F_{t-1,k}$ are known state transition matrices, and the Q_{tk} are known process covariance matrices.

Additionally, it is assumed that the signal components in the mixture distribution are also Gaussian, and that the means of these Gaussians are linearly related to the states of the signals k = 1, ..., M at times t = 1, ..., T, so that

$$G_k(\tau|x_{tk}) = \mathcal{N}(\tau; H_{tk} x_{tk}, R_{tk}), \qquad (2.25)$$

where the H_{tk} are known measurement matrices, and the R_{tk} are known measurement covariance matrices.

Finally, the background noise distribution in this application is assumed to be uniform and known for all t, so that the $G_0(\tau|x_{t0})$ terms are all constants.

With these assumptions, it is shown in reference 1 that for $X(k) = \{x_{0k}, x_{1k}, \ldots, x_{Tk}\}$, the value of X(k) that maximizes the auxiliary function Ψ_{kX} for each signal k is the solution to a symmetric, block-tridiagonal, linear system of equations, and that this system is most efficiently solved by a recursive Kalman smoothing filter. The details of this result are omitted here, but the filter steps are listed explicitly in the next section.

3. FREQUENCY TRACKER ALGORITHM STATEMENT

In the case of frequency tracking, the signal parameters of interest are typically instantaneous frequency γ_t and instantaneous frequency-rate $\dot{\gamma}_t$ at time t, so that for signal k,

$$x_{tk} = \begin{bmatrix} \gamma_{tk} \\ \dot{\gamma}_{tk} \end{bmatrix} . \tag{3.2}$$

For this two-state linear Markov model, the state transition matrices $F_{t-1,k}$ and the process covariance matrices $Q_{t-1,k}$ have simple forms:

$$F_{t-1,k} = \begin{bmatrix} 1 & \Delta_{t-1} \\ 0 & 1 \end{bmatrix}, \tag{3.3}$$

where Δ_t is the elapsed time between time t and time t-1, and

$$Q_{t-1,k} = q_{t-1,k} \begin{bmatrix} \frac{1}{3} \Delta_{t-1}^3 & \frac{1}{2} \Delta_{t-1}^2 \\ \frac{1}{2} \Delta_{t-1}^2 & \Delta_{t-1} \end{bmatrix},$$
(3.4)

where the $q_{t-1,k}$ are scale factors (see reference 5).

For a two-dimensional time-frequency display, the measurement matrices H_{tk} and the measurement covariance matrices R_{tk} also have simple forms:

$$H_{tk} = \begin{bmatrix} 1 & 0 \end{bmatrix}, \tag{3.5}$$

and

$$R_{tk} = \rho_{tk}^2, \tag{3.6}$$

where ρ_{tk}^2 is the variance of signal k at time t.

Let $\{\pi_{tk}^{(i)}\}$ be the set of estimated mixing proportions and $\{x_{tk}^{(i)}\}$ the set of estimated signal states at the *i*-th EM iteration. At the beginning of the algorithm (the 0-th iteration), the mixing proportions $\{\pi_{tk}^{(0)}\}$ are initialized so that $\pi_{tk}^{(0)} > 0$ and $\pi_{t0}^{(0)} + \pi_{t1}^{(0)} + \cdots + \pi_{tM}^{(0)} = 1$ for $t = 1, \ldots, T$. The signal state sequences $\{x_{0k}^{(0)}, x_{1k}^{(0)}, \ldots, x_{tM}^{(0)}\}$ are initialized with nominal values for $t = 1, \ldots, T$. For iterations $i = 0, 1, 2, \ldots$, the following nine quantities are computed:

1. Component bin probabilities for t = 1, ..., T, $\ell = 1, ..., L$, and k = 0, 1, ..., M:

$$P_{tk\ell}^{(i+1)} = \begin{cases} 1/L, & k = 0, \\ \int_{\ell} \mathcal{N}(\tau; H_{tk} x_{tk}^{(i)}, R_{tk}) d\tau, & k = 1, \dots, M. \end{cases}$$
(3.7)

2. Total bin probabilities for t = 1, ..., T and $\ell = 1, ..., L$:

$$P_{t\ell}^{(i+1)} = \sum_{k=0}^{M} \pi_{tk}^{(i)} P_{tk\ell}^{(i+1)}.$$
(3.8)

3. Total scan probabilities for t = 1, ..., T:

$$P_t^{(i+1)} = \sum_{\ell=1}^{L} P_{t\ell}^{(i+1)}.$$
 (3.9)

4. Bin centroids for t = 1, ..., T, $\ell = 1, ..., L$, and k = 1, ..., M:

$$\tilde{z}_{tk\ell}^{(i+1)} = \frac{1}{P_{tk\ell}^{(i+1)}} \int_{\ell} \tau \, \mathcal{N}(\tau; H_{tk} \, x_{tk}^{(i)}, R_{tk}) \, d\tau. \tag{3.10}$$

5. Synthetic measurements for t = 1, ..., T and k = 1, ..., M:

$$\tilde{z}_{tk}^{(i+1)} = \frac{\sum_{\ell=1}^{L} \left[z_{t\ell} \left(P_{tk\ell}^{(i+1)} / P_{t\ell}^{(i+1)} \right) \right] \tilde{z}_{tk\ell}^{(i+1)}}{\sum_{\ell=1}^{L} \left[z_{t\ell} \left(P_{tk\ell}^{(i+1)} / P_{t\ell}^{(i+1)} \right) \right]}.$$
(3.11)

6. Synthetic measurement covariance matrices for t = 1, ..., T and k = 1, ..., M:

$$\tilde{R}_{tk}^{(i+1)} = \frac{R_{tk}}{\pi_{tk}^{(i)} \sum_{\ell=1}^{L} z_{t\ell}^{(i+1)} \left(P_{tk\ell}^{(i+1)} / P_{t\ell}^{(i+1)} \right)}.$$
(3.12)

7. Synthetic process covariance matrices for t = 0, 1, ..., T - 1 and k = 1, ..., M:

$$\tilde{Q}_{tk}^{(i+1)} = \frac{P_t^{(i+1)}}{\|Z_t\|} Q_{tk}. \tag{3.13}$$

8. Estimated mixing proportions for t = 1, ..., T and k = 0, 1, ..., M:

$$\pi_{tk}^{(i+1)} = \frac{\pi_{tk}^{(i)} \sum_{\ell=1}^{L} z_{t\ell}^{(i+1)} \left(P_{tk\ell}^{(i+1)} / P_{t\ell}^{(i+1)} \right)}{\sum_{k'=1}^{M} \pi_{tk'}^{(i)} \sum_{\ell=1}^{L} \left(P_{tk'\ell}^{(i+1)} / P_{t\ell}^{(i+1)} \right)}.$$
 (3.14)

9. Estimated signal states for $t=0,1,\ldots,T$ and $k=1,\ldots,M$, using (for computational efficiency) a recursive Kalman smoothing filter, which comprises a forward filter initialized at time t=0 with $\tilde{y}_{0|0}^{(i+1)}(k)=x_{0k}^{(0)}$ and a large (diffuse) state covariance matrix $P_{0|0}^{(i+1)}(k)$, and given, for $t=0,1,\ldots,T-1$, by the recursions

$$P_{t+1|t}^{(i+1)}(k) = F_{tk} P_{t|t}^{(i+1)}(k) F_{tk}^* + Q_{tk}, \tag{3.15}$$

$$W_{t+1}^{(i+1)}(k) = P_{t+1|t}^{(i+1)}(k) H_{t+1,k}^* \left[H_{t+1,k} P_{t+1|t}^{(i+1)}(k) H_{t+1,k}^* + R_{t+1,k} \right]^{-1}, \quad (3.16)$$

$$P_{t+1|t+1}^{(i+1)}(k) = P_{t+1|t}^{(i+1)}(k) - W_{t+1}^{(i+1)}(k) H_{t+1,k} P_{t+1|t}^{(i+1)}(k),$$
(3.17)

$$\tilde{y}_{t+1|t+1}^{(i+1)}(k) = F_{tk} \, \tilde{y}_{t|t}^{(i+1)}(k) + W_{t+1}^{(i+1)}(k) \left[\tilde{z}_{t+1,k}^{(i+1)} - H_{t+1,k} \, F_{tk} \, \tilde{y}_{t|t}^{(i+1)}(k) \right], \quad (3.18)$$

and a backward filter initialized at time t = T with $x_{Tk}^{(i+1)} = \tilde{y}_{T|T}^{(i+1)}(k)$ and given, for t = T - 1, T - 2, ..., 1, by the recursion

$$x_{tk}^{(i+1)} = \tilde{y}_{t|t}^{(i+1)}(k) + P_{t|t}^{(i+1)}(k) F_{tk}^* \left(P_{t+1|t}^{(i+1)}(k) \right)^{-1} \left[x_{t+1,k}^{(i+1)} - F_{tk} \, \tilde{y}_{t|t}^{(i+1)}(k) \right], \tag{3.19}$$

and, for t=0, by

$$x_{0k}^{(i+1)} = F_{0k}^{-1} x_{1k}^{(i+1)}, (3.20)$$

where the asterisk denotes matrix transposition.

The most common convergence tests for termination of the algorithm are based on the rate of increase of the incomplete data likelihood function. Other tests are based on the rate of change of the estimated parameters. In practice, usually some combination of these two tests is used.

4. EXAMPLES

4.1 LINEAR CHIRP

In this section, a two-state histogram-PMHT frequency tracker is used to track the instantaneous frequency and frequency-rate of a low-frequency linear chirp.

Consider the continuous-time, complex-sinusoidal signal x(t) with constant amplitude A, constant phase ϕ , and time-varying instantaneous frequency $\gamma(t)$,

$$x(t) = A \exp[i 2\pi \gamma(t) t + i \phi], \tag{4.2}$$

where

$$\gamma(t) = \gamma_0 + \dot{\gamma}_0 t, \tag{4.3}$$

 γ_0 is the nominal frequency in Hz, and $\dot{\gamma}_0$ is the chirp-rate in Hz/s. Converting to radians, equations (4.2) and (4.3) are rewritten as

$$x(t) = A \exp[i\Omega(t) t + i\phi], \tag{4.4}$$

and

$$\Omega(t) = \Omega_0 + \dot{\Omega}_0 t, \tag{4.5}$$

where $\Omega(t)$ is the instantaneous frequency in rad/s, Ω_0 is the nominal frequency in rad/s, and $\dot{\Omega}_0$ is the chirp-rate in rad/s².

Without loss of generality, it is assumed that the signal is observed starting at time t = 0, and that estimates of the instantaneous frequency and frequency-rate of x(t) are required every \mathcal{T} seconds. To avoid aliasing, the signal is sampled well above the Nyquist rate for the observation period of interest $S\mathcal{T}$, where S is the number of scans; that is

$$\Omega_s = \frac{2\pi}{\mathcal{T}_s} \gg 2\,\Omega(S\mathcal{T}),\tag{4.6}$$

where Ω_s is the sampling rate in rad/s, and \mathcal{T}_s is the sampling period in seconds. Using n to denote the sampling index, the discrete-time versions of equations (4.4) and (4.5) are given by

$$x(n\mathcal{T}_s) = A \exp[i\Omega(n\mathcal{T}_s) n\mathcal{T}_s + i\phi]$$

$$x[n] = A \exp(i\omega[n] n + i\phi), \tag{4.7}$$

and

$$\mathcal{T}_{s} \Omega(n\mathcal{T}_{s}) = \mathcal{T}_{s} \Omega_{0} + \mathcal{T}_{s} \dot{\Omega}_{0} n \mathcal{T}_{s}$$

$$\omega[n] = \omega_{0} + \dot{\omega}_{0} n, \qquad (4.8)$$

for n = 0, ..., N-1, where $\omega[n]$ is the instantaneous frequency in rad/sample, ω_0 is the nominal frequency in rad/sample, and $\dot{\omega}_0$ is the chirp-rate in rad/sample² (see reference 6 for details on time-sampling).

For simplicity, it is assumed that the signal x(t) is corrupted by additive, complex, zero-mean white Gaussian noise with variance σ^2 , denoted $v(t) \sim \mathcal{CN}(0, \sigma^2)$; that is, the observed time-series is given by

$$y[n] = x[n] + v[n],$$
 (4.9)

where

$$E\{v[n]\} = 0, (4.10)$$

$$E\{v[n] \ v[n+k]\} = \sigma^2 \delta[k], \tag{4.11}$$

for all n and k. An observation interval of length \mathcal{T} seconds and a sampling period of length \mathcal{T}_s seconds yields a time-series of length $\mathcal{T}/\mathcal{T}_s+1$ samples every \mathcal{T} seconds, for a total of $N=S(\mathcal{T}/\mathcal{T}_s+1)$ samples.

For each observation interval, the signal-to-noise ratio (SNR) η is defined as the ratio of the average signal power P to the total noise power σ^2 ,

$$\eta \equiv \frac{P}{\sigma^2} \tag{4.12}$$

For the signal of interest, the average signal power $P = A^2$, so $\eta = A^2/\sigma^2$.

In these simulation examples, a low-frequency linear chirp with amplitude A=1, phase $\phi=0$, nominal frequency $\gamma_0=20$ Hz, and chirp-rate $\dot{\gamma}_0=0.125$ Hz/s is sampled every $\mathcal{T}_s=0.0125$ second, and its short-time Fourier transform (STFT) is taken every $\mathcal{T}=1$ second for S=120 consecutive, nonoverlapping (unaveraged) blocks of data (scans) to yield a spectrogram of length $S\mathcal{T}=2$ minutes. This sampling period corresponds to a sampling rate of $\gamma_s=1/\mathcal{T}_s=80$ Hz, which is well above the Nyquist rate of $2\gamma(S\mathcal{T})=2\left[\gamma_0+\dot{\gamma}_0(S\mathcal{T})\right]=70$ Hz for the 2-minute observation period. Each 1-second observation interval yields $\mathcal{T}/\mathcal{T}_s+1=81$ samples, for a total of N=9720 samples over the whole data set.

The spectrogram of the noise-free ($\sigma=0$) signal is shown in figure 1. The spectrograms for signals with $\sigma=A$ (0 dB), 3A (-9.5424 dB), 5A (-13.9794 dB), and 6A (-15.5630 dB) are shown in figures 3, 5, 7, and 9, respectively.

The STFTs in these examples are computed using a 128-point fast Fourier transform (FFT) and an 81-point Hanning window. The window sequence is normalized such that it sums to one; this scaling allows the magnitude-squared FFT output to be directly interpreted as power. Since for a P-point DFT the spacing between DFT frequencies is $2\pi/P$, and the

relationship between the discrete-time frequency ω and the continuous-time frequency Ω is $\omega = \Omega \mathcal{T}_s$, where \mathcal{T}_s is the sampling period, the frequency resolution is given by $2\pi/P\mathcal{T}_s$ rad/s, so the DFT bin-width for this example is $1/(128 \times 0.0125) = 0.625$ Hz. Only the positive half of the spectrum is shown in figure 1, and only the first L = 64 bins of sensor data are considered in the sequel.

The effect of the window is to smear the signal in time and frequency, and hence add to the apparent bandwidth of the signal induced by the spectral sampling. While windowing decreases the resolution of the spectrogram, it would seem to improve the fit of the mixture model to the data in this case—the broadening effect of the window adds "variance" to the signal. Although this smearing of the signal by the window is a purely deterministic effect, it is treated as a stochastic effect by the histogram-PMHT tracker; that is, the width of the signal is modeled by the variance of the signal component of the mixture.

The histogram-PMHT frequency tracker outlined in section 3 was implemented as a single-scan (T=1), single-signal (M=1) sequential filter and was applied to the data in figures 1, 3, 5, 7, and 9, on a per-scan basis; that is, the scans were processed sequentially, where the estimate for the previous scan was used to initialize the estimate for the current scan (see reference 1). The values used for $q_{t-1}=q$ and $\rho_t=\rho$ in equations (3.4) and (3.6) are listed in the figure captions.

The estimated instantaneous frequencies are shown connected by a solid line in each figure. The tracks become increasingly jagged as the SNR drops and the signal power varies more from cell to cell. The jaggedness of the tracks is also a function of the process noise: the stochastic signal model allows for further excursions from the deterministic, constant-rate model as the process noise scale factor q is increased, resulting in larger random accelerations. There is an intimate relationship between the values of the filter parameters ρ and q, the SNR, the track initialization, and the tracker behavior. High SNR signals will tend to draw the signal component of the mixture closer if the signal is within the effective "gate" determined by ρ . The amount by which the signal component will move to data outside the range of the deterministic process model depends on the SNR, the value of q, and the track's local estimate of its own quality (i.e., the size of the state covariance $P_{t|t}$ on x_t). In low SNR, the "inertia" of the tracker will allow it to coast according to the deterministic process model until there is good reason (i.e., supporting data) for it to change course.

The track in figure 9 was terminated prematurely because it had lost track. Because the nearest peak in the second scan of data is far to the left of where the track was initialized (at 21.875 Hz, the right edge of bin 35), a large innovation was generated in the filter, which led to a large negative frequency-rate estimate from which the tracker never recovered. In the absence of consistently strong data, the tracker coasted according to its current rate estimate, with minor course corrections in the vicinity of strong local peaks. This example is a good example of where a multi-scan batch filter would be beneficial. A batch of, say, 10 scans in this example would probably provide enough smoothing for an acceptable initial

track estimate. The batch estimate could then be used to either initialize the next batch, slid forward by one scan, or to initialize a single-scan sequential tracker like the one used in these examples.

Plots of the instantaneous frequency and frequency-rate estimates for these examples, along with the true frequencies and frequency-rate, are shown in figures 2, 4, 6, and 8. The apparent small (less than one bin-width) bias in the frequency estimates is thought to be due more to a combination of the resolution of the STFT, and the known bias of the windowed periodogram (see reference 6), than to the tracker. The histogram-PMHT tracker is a maximum likelihood estimator, and should therefore be asymptotically unbiased, efficient, and normal. A detailed statistical analysis of histogram-PMHT performance has not yet been done, and is left for future work.

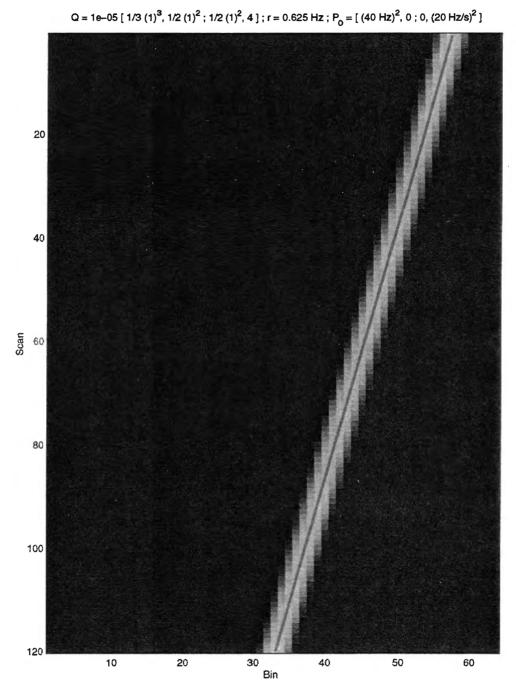


Figure 1. Magnitude-Squared STFT of Noise-Free Linear Chirp ($\eta=\infty$ dB, $\rho=1$ Bin (0.625 Hz), $q=1\times 10^{-5}$) and Estimated Track

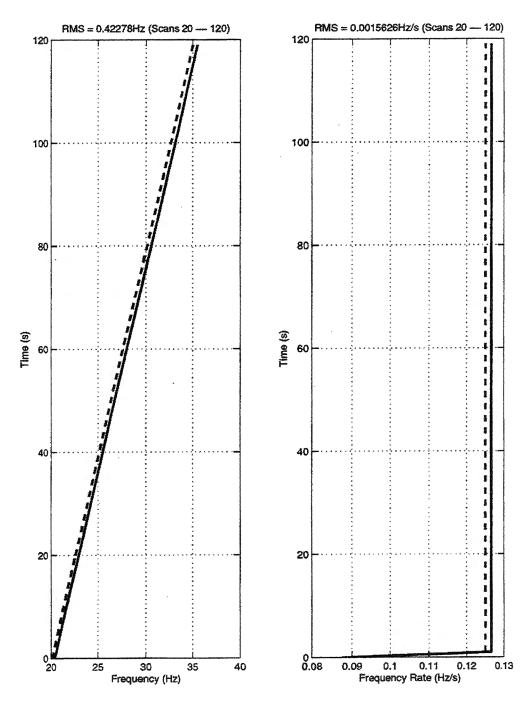


Figure 2. Estimated and True Instantaneous Frequencies and Frequency-Rates for a Noise-Free Linear Chirp $(\eta = \infty \ dB, \ \rho = 1 \ Bin \ (0.625 \ Hz), \ q = 1 \times 10^{-5})$

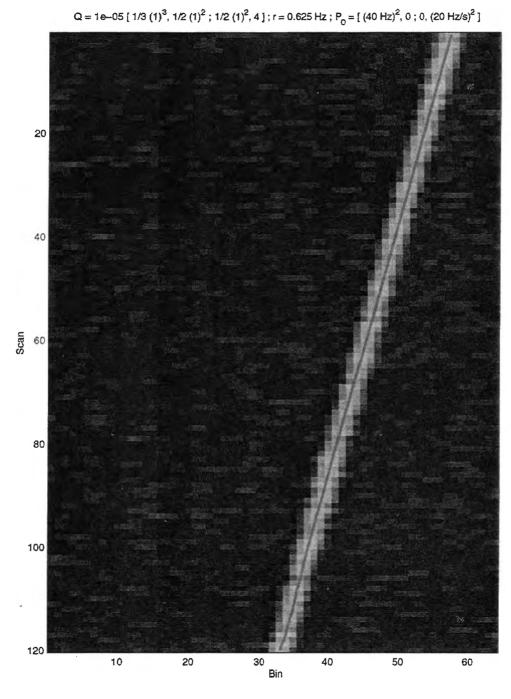


Figure 3. Magnitude-Squared STFT of Linear Chirp in White Gaussian Noise ($\eta=0$ dB, $\rho=1$ Bin (0.625 Hz), $q=1\times 10^{-5}$) and Estimated Track

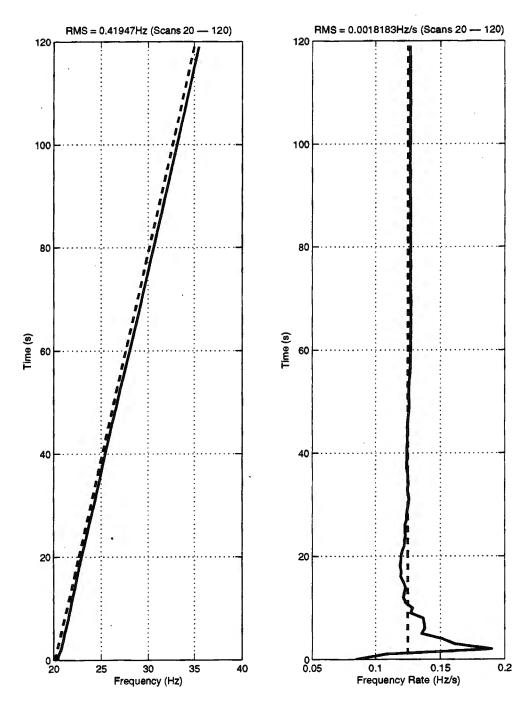


Figure 4. Estimated and True Instantaneous Frequencies and Frequency-Rates for a Linear Chirp in White Gaussian Noise ($\eta=0$ dB, $\rho=1$ Bin (0.625 Hz), $q=1\times 10^{-5}$)

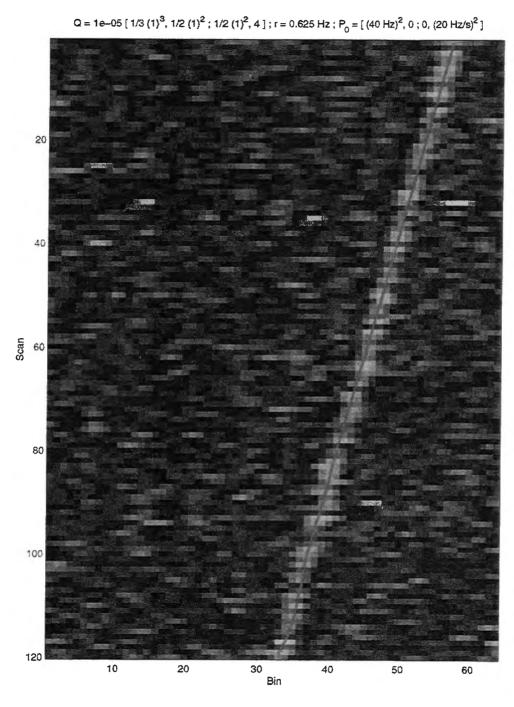


Figure 5. Magnitude-Squared STFT of Linear Chirp in White Gaussian Noise $(\eta=-9.5424~\text{dB},~\rho=1~\text{Bin}~(0.625~\text{Hz}),~q=1\times10^{-5})$ and Estimated Track

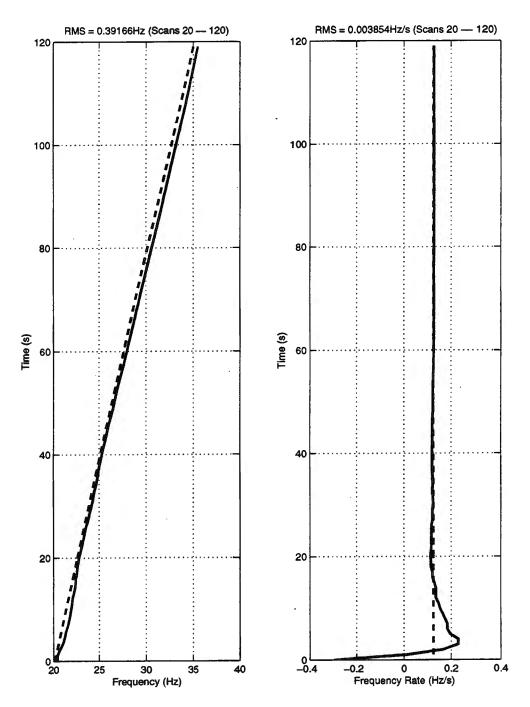


Figure 6. Estimated and True Instantaneous Frequencies and Frequency-Rates for a Linear Chirp in White Gaussian Noise ($\eta=-9.5424$ dB, $\rho=1$ Bin (0.625 Hz), $q=1\times 10^{-5}$)

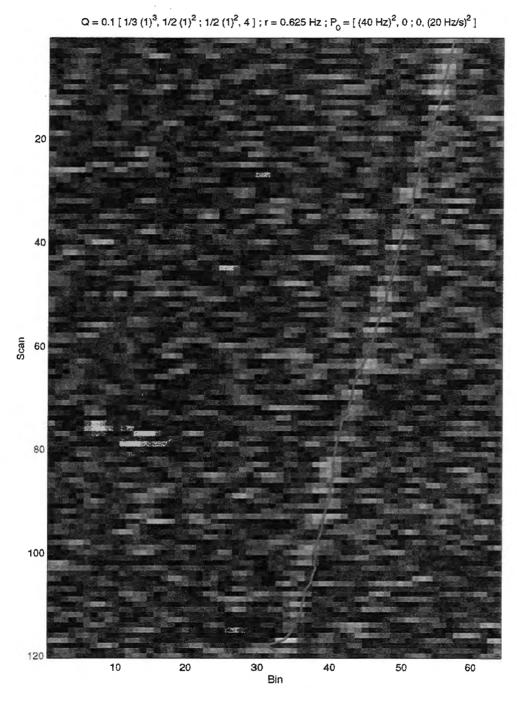


Figure 7. Magnitude-Squared STFT of Linear Chirp in White Gaussian Noise $(\eta=-13.9794~dB,~\rho=1~Bin~(0.625~Hz),~q=1\times10^{-3})$ and Estimated Track

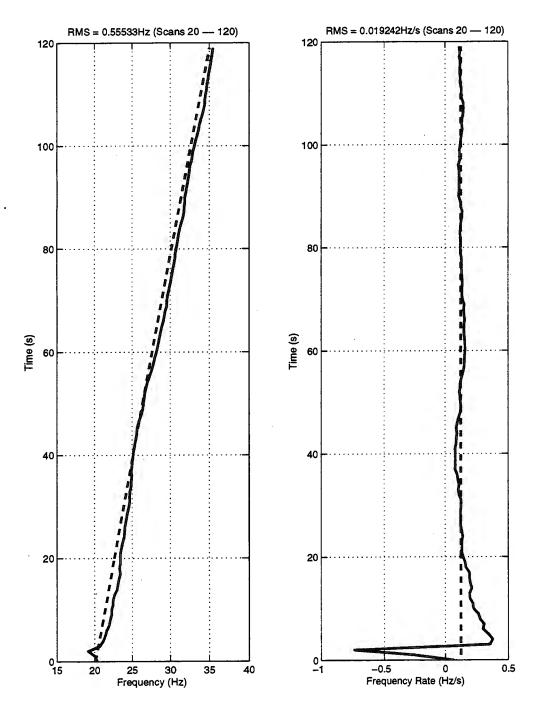


Figure 8. Estimated and True Instantaneous Frequencies and Frequency-Rates for a Linear Chirp in White Gaussian Noise ($\eta = -13.9794$ dB, $\rho = 1$ Bin (0.625 Hz), $q = 1 \times 10^{-3}$)

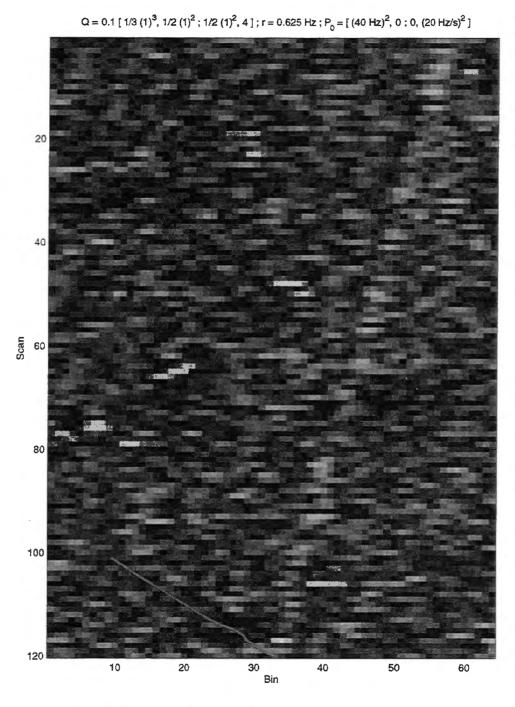


Figure 9. Magnitude-Squared STFT of Linear Chirp in White Gaussian Noise $(\eta=-15.5630$ dB, $\rho=1$ Bin (0.625 Hz), $q=1\times10^{-3})$ and Estimated Track

4.2 BOWHEAD WHALE CALL

The spectrogram of a 1.2-second bowhead whale call recorded at sea is shown in figure 10. This signal was sampled at 2500 Hz and processed with a 421-point Chebyshev window and a 1024-point FFT with a bin resolution of 2.4414 Hz. Values of $\rho = 3$ bins (7.3242 Hz) and $q = 1 \times 10^{-3}$ were used to track this signal. The estimated instantaneous frequencies are shown connected by a solid line in figure 10.

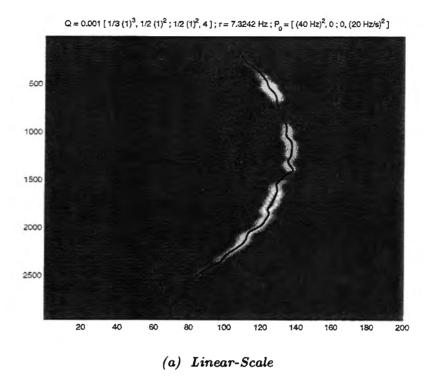
The intent of this example is to show the ability of the tracker to track very complex, non-stationary signals, and the ability of the stochastic process model to accommodate dynamics of higher order than the deterministic process model. The benefit of including process noise is the ability to track high dynamics with a reduced parameter set. However, for too low a model order, the burden of tracking the signal dynamics falls squarely on the shoulders of the process noise, and the result for high process noise may be very jagged tracks or, for low processes noise, tracks whose dynamics lag those of the actual track. The appropriate model order and process noise level are of course application dependent.

5. CONCLUDING REMARKS

The histogram-PMHT tracking methodology avoids the thorny issues of thresholding the sensor data to provide measurements for a point tracker by (1) using all of the sensor data, and (2) modeling the signals as potentially distributed over several cells. The histogram-PMHT signal model is a stochastic model in that the signal centers are modeled as the component means of a discrete mixture distribution; the signal "bandwidths" are modeled by the variances of the mixture components.

The interpretation of the sensor output as a pseudo-histogram plays an important role in the derivation of histogram-PMHT. The real-valued cell outputs are quantized and treated as the cell counts of a pseudo-histogram whose distribution is multinomial; the underlying density of this multinomial distribution is the mixture density of the signals and the background noise. It is a remarkable fact that the sensor data are recovered in the algorithm as the quantization level \hbar^2 is taken to zero.

Several extensions to histogram-PMHT exist, and some of these are developed in reference 1. For instance, the measurement covariance matrices R_{tk} and the process covariance matrices Q_{tk} can be treated as unknowns and estimated from the data. Also, some of the unknowns can be linked together parametrically or held fixed, if either option makes sense in the application. For example, the process covariance matrices Q_{tk} and the mixing proportions π_{tk} can be held constant for each signal over all scans such that $Q_{tk} = Q_k$ and $\pi_{tk} = \pi_k$ for all t and t.



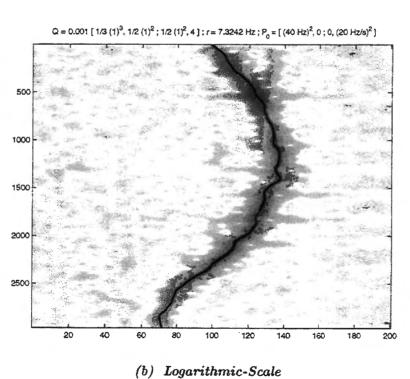


Figure 10. Spectrogram of Bowhead Whale Call

Another important theoretical development in the derivation of histogram-PMHT not discussed in this paper is the use of a negative multinomial distribution (see reference 4) to model sensor cells in which no data are collected. The negative multinomial functions as an interpolator in this case, serving to restore the missing cell counts in the pseudo-histogram. In this capacity, the negative multinomial may be useful to reduce "edge effects" that may bias estimates when the tails of signal components extend beyond the ends of the sensor display. The reader is referred to reference 1 for further details on the use of the negative multinomial in histogram-PMHT.

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